

FACULTY OF ENGINEERING AND SPATIAL SCIENCE DEPARTMENT OF MINING AND PROCESS ENGINEERING

| QUALIFICATION: BACHELORS OF ENGINEERING IN MINING ENGINEERING | | | | |
|---|-----------------------------|--|--|--|
| QUALIFICATION CODE: BEMIN | LEVEL: 6 | | | |
| COURSE CODE: RMC711S | COURSE NAME: ROCK MECHANICS | | | |
| SESSION: JUNE 2022 | PAPER: THEORY | | | |
| DURATION: 3 HOURS | MARKS: 100 | | | |

| | FIRST OPPORTUNITY QUESTION PAPER |
|-------------|----------------------------------|
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| MODERATOR: | Prof. Mapani Benjamin |

| INSTRUCTIONS | | | | |
|---|--|--|--|--|
| Answer all questions. | | | | |
| 2. Read all the questions carefully before answering. | | | | |
| 3. Marks for each question are indicated at the end of each question. | | | | |
| 4. Please ensure that your writing is legible, neat and presentable. | | | | |

PERMISSIBLE MATERIALS

- 1. Examination paper.
- 2. Two Graph Papers
- 3. Mathematical Instruments

THIS QUESTION PAPER CONSISTS OF 4 PAGES (Including this front page)



Instructions: Answer Question 1 and any 4 other questions. Excess questions will not be marked.

Question 1 is compulsory.

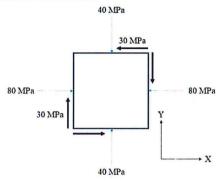
Time allowed: 3 hours

| Question 1 | Short answer questions | (20) |
|------------|---|------|
| a) | What the difference between rock and rock mass? | |
| b) | What is the range of 'Q' value in 'Q' classification system? | |
| c) | What is the maximum length of drill core run used to measure RQD? | |
| d) | How do the water in the joints influence the stability of rock mass? | |
| e) | Which side the Mohr's circle moves when pore pressure is increased? | |
| f) | What are the parameters associated with Bieniawski's RMR? | |
| g) | Direction of major principal stress for a rock is 35° from x-axis. What is the major shear stress direction with respect to y-axis [both x, y-axes are perpendicular to each other] | |
| h) | RQD is the first quantitative rock mass classification system developed by John Deer [1964]. Nevertheless, it has two major problems with respect to rock mass classification, what are they? | |
| i) | In triaxial testing, which of confining stress and axial stress, is constant? | |
| j) | Shear strength failure criteria for a rock sample is $\tau = 25 + \sigma_n$ Tan 23.6°, then what is the angle between failure plane and major principal stress direction? [2] | |
| Question 2 | Briefly discuss the following characteristics of discontinuities and their effect on stability of rockmass with diagrams wherever possible a) Joint spacing b) Joint orientation c) Fracture aperture d) Fracture roughness e) Fracture filling | (20) |
| Question 3 | A competent sandstone rock mass is fractured by three joint sets plus random fractures. The average RQD is 75%; the average joint spacing is 0.18 m. The joint surfaces are slightly rough and slightly weathered. The joints are in contact with apertures generally less than 1 mm; no clay is found on the surfaces. The point load strength index of the sandstone is 3.5 MPa. The tunnel is to be excavated at 50 m below the ground level and the ground water table is 20 m below the ground surface, thus large inflow of water expected. Estimate the Q-value. | (20) |
| Question 4 | | |
| a) | What are methods used to measure in situ stresses and classify them according to the amount of disturbance caused during measurement | (6) |
| b) | Briefly describe with help of figures, in situ stress measurement using flatjack method | (14) |

(14)

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Question 5 The state of stress in a rockmass is represented as shown in Fig. 1. Employ Mohr's circle to determine (a) the magnitude and orientation of the principal stresses with respect of x-direction and (b) the magnitude and orientation of the maximum shear stress with respect to x-direction and associated normal stresses.



Question 6

- a) What are the limitations of Mohr Coulomb failure criteria?
- (8) resses at (12)
- b) In a series of triaxial compression test on sandstone, the following represent the stresses at peak load conditions.

| Test | σ ₃ (MPa) | σ ₁ (MPa) |
|------|----------------------|----------------------|
| 1 | 10 | 99.2 |
| 2 | 20 | 129.3 |
| 3 | 30 | 160 |
| 4 | 40 | 189.1 |

Determine cohesion and angle of internal friction that best fit the data

Table 1. Description and ratings for the input parameters of the Q-system (simplified from Grimstad and Barton, 1993).

Jn (joint set number)

| ROD | (Rock | Quality | Designa | tion |
|-----|-------|---------|---------|------|
| | | | | |

| NGD [Nock Quality D | esignation |
|---------------------|---------------|
| Very poor | RQD = 0 - 25% |
| Poor | 25 - 50 |
| Fair Good | 50 - 75 |
| Good | 75 - 90 |
| Excellent | 90 - 100 |
| Notes: | |

(i) Where RQD is reported or measured as < 10 (including 0), a nominal value of 10 is used to evaluate Q

(ii) RQD intervals of 5, i.e. 100, 95, 90, etc. are sufficiently accurate

| Massive, no or few joints | Jn = 0.5 - 1 |
|--|--------------|
| One joint set | 2 |
| One joint set plus random joints | 3 |
| Two joint sets | 4 |
| Two joint sets plus random joints | 6 |
| Three joint sets | 9 |
| Three joint sets plus random joints | 12 |
| Four or more joint sets, heavily jointed, "sugar-cube", etc. | 15 |
| Crushed rock, earthlike | 20 |
| Notes: (i) For tunnel intersections, use (3.0 x Jn); (ii) For portals, use (| (2.0 x Jn) |

Jr (joint roughness number)

| a) Rock-wall contact, b) rock-wall contact before 10 cm | shear | c) No rock-wall contact when sheared | |
|---|-------|---|----------|
| Discontinuous joints Jr = 4 | | Zone containing clay minerals thick enough to prevent rock- | Jr = 1.0 |
| Rough or irregular, undulating | 3 | wall contact | |
| Smooth, undulating | 2 | Sandy, gravelly or crushed zone thick enough to prevent rock- wall contact | |
| Slickensided, undulating | 1.5 | | |
| Rough or irregular, planar | 1.5 | Notes: | |
| Smooth, planar | 1.0 | i) Add 1.0 if the mean spacing of the relevant joint set is greater than 3 m | |
| Slickensided, planar | 0.5 | ii) Jr = 0.5 can be used for planar, slickensided joints having lineations, | |
| Note : i) Descriptions refer to small scale fe and intermediate scale features. in t | | provided the lineations are oriented for minimum strength | |

Ja (joint alteration number)

| en | JOINT WA | ALL CHARACTER | | Condition | Wall contact | | |
|--------------------|---------------------|--------------------|--|--|------------------------|-----------------|--|
| between walls | | Healed o | welded joints: filling of quartz, epidote, etc. | | | Ja = 0.75 | |
| betwe walls | CLEAN JOINTS | Fresh joir | nt walls: | no coating or filling, except from staining (rust) | | 1 | |
| itact | | Slightly a | Itered joint walls: | non-softening mineral coatings, cla | y-free particles, etc. | 2 | |
| ontact joint | COATING OR THIN | Friction n | naterials: | terials: sand, silt, calcite, etc. (non-softening) | | | |
| ပိ | FILLING | Cohesive | materials: | aterials: clay, chlorite, talc, etc. (softening) | | | |
| wall | | | | | Some wall contact | No wall contact | |
| | FILLING O | F: | | Туре | Thin filling (< 5 mm) | Thick filling | |
| e or no contact | Friction materials | sand, silt calcite | | sand, silt calcite, etc. (non-softening) | | Ja = 8 | |
| e or | Hard cohesive mate | erials | compacted filling of clay, chlorite, talc, etc. | | 6 | 5 - 10 | |
| ome | Soft cohesive mate | rials | medium to low overconsolidated clay, chlorite, talc, | | 8 | 12 | |
| S | Swelling clay mater | ials | filling material e | exhibits swelling properties | 8 - 12 | 13 - 20 | |

Jw (joint water reduction factor)

| Dry excavations or minor inflow, i.e. < 5 l/min locally | $p_w < 1 \text{ kg/cm}^2$ | Jw = 1 |
|---|---------------------------|------------|
| Medium inflow or pressure, occasional outwash of joint fillings | 1 - 2.5 | 0.66 |
| Large inflow or high pressure in competent rock with unfilled joints | 2.5 - 10 | 0.5 |
| Large inflow or high pressure, considerable outwash of joint fillings | 2.5 - 10 | 0.3 |
| Exceptionally high inflow or water pressure at blasting, decaying with time | > 10 | 0.2 - 0.1 |
| Exceptionally high inflow or water pressure continuing without noticeable decay | > 10 | 0.1 - 0.05 |
| Note: (i) The last four factors are crude estimates. Increase Jw if drainage measures are installed | • | |
| (ii) Special problems caused by ice formation are not considered | | |

SRF (Stress Reduction Factor)

| Weakness zones intersecting excavation | Multiple weakness zones with clay or chemically disintegrated rock, very loose surrounding rock (any depth) | | | SRF = 10 | |
|--|---|-----------------------------------|---------------------------------|--------------------------------|-----------|
| | Single weakness zones containing clay or chemically disintegrated rock (depth of excavation < 50 m) | | | 5 | |
| | Single weakness zones containing clay or chemically disintegrated rock (depth of excavation > 50 m) | | | 2.5 | |
| | Multiple shear zones in competent rock (clay-free), loose surrounding rock (any depth) | | | 7.5 | |
| | Single shear zones in competent rock (clay-free), loose surrounding rock (depth of excavation < 50 m) | | | 5 | |
| | Single shear zones in competent rock (clay-free), loose surrounding rock (depth of excavation > 50 m) | | | 2.5 | |
| | Loose, open joints, heavily jointed or "sugar-cube", etc. (any depth) | | | 5 | |
| Note: (i) Reduce these SRF values by 25 - 50% if the relevant shear zones only influence, but do not intersect the excavation. | | | | | |
| | | | $\sigma_{\rm c}/\sigma_{\rm 1}$ | $\sigma_{\theta} / \sigma_{c}$ | SRF |
| Competent rock, rock stress problems | Low stress, near surface, open joints | | > 200 | < 0.01 | 2.5 |
| | Medium stress, favourable stress condition | | 200 - 10 | 0.01 - 0.3 | 1 |
| | High stress, very tight structure. Usually favourable to stability, may be except for walls | | | 0.3 - 0.4 | 0.5 - 2 |
| | Moderate slabbing after > 1 hour in massive rock 5 - 3 0.5 - 0.65 | | | 5 - 50 | |
| | Slabbing and rock burst after a few minutes in massive rock 3 - 2 0.65 - 1 | | | 50 - 200 | |
| | Heavy rock burst (strain burst) and immediate dynamic deformation in massive rock | | < 2 | > 1 | 200 - 400 |
| Notes: (ii) For strongly anisotropic stress field (if measured): when $5 < \sigma_1/\sigma_3 < 10$, reduce σ_c to $0.75 \sigma_c$. When $\sigma 1/\sigma_3 > 10$, reduce σ_c to $0.5 \sigma_c$ | | | | | |
| (iii) Few case records available where depth of crown below surface is less than span width. Suggest SRF increase from 2.5 to 5 for low stres | | | | | |
| σ_0/σ_c | | | | σ_0 / σ_c | SRF |
| Squeezing | Plastic flow of incompetent rock under | Mild squeezing rock pressure | | 1 - 5 | 5 - 10 |
| rock the influence of high pressure | | Heavy squeezing rock pressure > 5 | | 10 - 20 | |
| Swelling Chemical swelling activity depending on | | Mild swelling rock pressure | | | 5 - 10 |
| rock presence of water | | Heavy swelling rock pressure | | | 10 - 15 |

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